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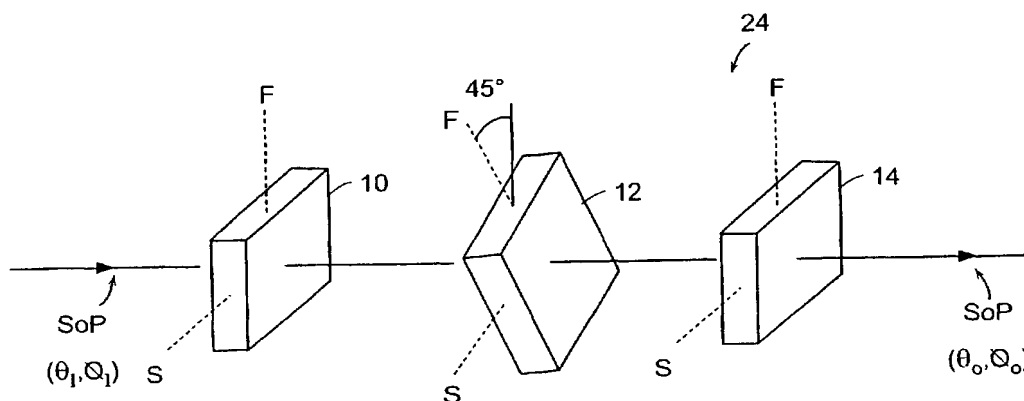
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(54) Title: POLARIZATION TRANSFORMER



(57) Abstract: A polarization transformer includes at least one plate of transparent polycrystalline material which has an optical axis oriented perpendicular to a propagation direction of incident radiation having a first polarization state. The plate includes electrodes for applying an electric field across a plane of the plate perpendicular to the propagation direction so as to provide controlled phase change such that the polarization of radiation transmitted through the polarization transformer is transformed from the first polarization state to a second polarization state. The plate in a preferred embodiment comprises a ferroelectric complex oxide such as lead lanthanum zirconate titanate (PLZT) material. Such a material provides devices that have very fast response (on the order of microseconds) and low insertion loss.

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POLARIZATION TRANSFORMER

RELATED APPLICATIONS

This application is a continuation-in-part of and claims priority to Application No. 09/519,293 filed 6 March 2000, the teachings of which are
5 incorporated herein by reference in their entirety.

BACKGROUND OF THE INVENTION

Transformation of the state of polarization (SoP) of light beams is important in many applications. For example, fiber optic communication systems often include optical devices that are sensitive to the direction at which light is polarized.
10 Yet typical optical fibers do not preserve the state of polarization. Further, the different polarization directions can have different propagation velocities (birefringence) and thus can contribute to the degradation of optical communication signals. To counter this deleterious effect known as polarization mode dispersion, a polarization transformer can be used to actively adjust the polarization state of the
15 incoming light signal so that a corrective differential delay can be applied and thereby correct for the velocity mismatch.

Much progress has been made in the development of polarization transformers, but current devices are not very satisfactory for many applications. In many applications, it is desirable that such devices have fast response time and low
20 insertion loss. The current devices include integrated optical waveguides, liquid crystal-based devices and optical fiber-based devices.

The integrated optical waveguides are typically made of lithium niobate and can include an input phase shifter section, a polarization converter section and an output phase shifter section. These waveguides have very fast response times;
25 however, such devices have high insertion loss and are expensive to produce.

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The liquid crystal-based devices include nematic liquid crystal cells whose birefringence is controlled using an external voltage. The liquid crystal devices are slower than the lithium niobate waveguides and are difficult to control in intermediate states. Although it has the desirable features of low insertion loss and low required operating voltage, the long term reliability of organic materials and the relatively low switching speed of a liquid crystal-based device are not suitable for many applications.

The optical fiber based devices use a fiber loop arrangement which operates according to the principle that changing the relative plane of the fiber loops changes the polarization state at the output. The fiber loop devices have very low insertion loss but are the slowest of the three current device types.

SUMMARY OF THE INVENTION

There is a need for an approach to fabrication of polarization transformers which provides devices that have very fast response time and low insertion loss.

Accordingly, an embodiment of a polarization transformer comprises at least one plate of transparent polycrystalline material which has an optical axis oriented perpendicular to a propagation direction of incident radiation having a first polarization state. The at least one plate includes electrodes for applying an electric field across a plane of the plate perpendicular to the propagation direction so as to provide controlled phase change such that the polarization of radiation transmitted through the polarization transformer is transformed from the first polarization state to a second polarization state. The plate in a preferred embodiment comprises a ferroelectric complex oxide such as lead lanthanum zirconate titanate (PLZT) material. Such a material provides devices that have very fast response (on the order of microseconds) and low insertion loss.

According to an aspect of the material, the plate is isotropic in the absence of an applied electric field across the plate electrodes. An electric field corresponding to an applied voltage less than 400 volts provides a phase retardation of about 180 degrees.

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In accordance with another embodiment, the polarization transformer comprises first and second plates disposed such that the incident radiation is transmitted through the two plates and the orientation of an optical axis of the second plate is at an angle such as 45 degrees with respect to the optical axis of the first plate.

In accordance with yet another embodiment, the polarization transformer comprises first, second and third plates disposed such that the incident radiation is transmitted through the three plates and the orientation of an optical axis of the second plate is at 45 degrees with respect to the optical axis of the first and third plates.

According to an another aspect, the polarization transformer is capable of transforming a first arbitrary polarization state at its input to a second arbitrary polarization state at its output.

A preferred embodiment of the invention includes a polarization transformer in an optical communication system including an input optical fiber, an input optical coupling, a polarization transformer, an output optical coupling and an output optical fiber.

BRIEF DESCRIPTION OF THE DRAWINGS

The foregoing and other objects, features and advantages of the invention will be apparent from the following more particular description of preferred embodiments of the invention, as illustrated in the accompanying drawings in which like reference characters refer to the same parts throughout the different views. The drawings are not necessarily to scale, emphasis instead being placed upon illustrating the principles of the invention.

FIG. 1 is a schematic diagram illustrating an embodiment of a polarization transformer having a single plate.

FIG. 2 is a perspective view illustrating an embodiment of a plate for use in the polarization transformer embodiment of FIG. 1.

FIG. 3 is a schematic diagram illustrating an embodiment of a polarization transformer having two plates wherein the orientation of an optical axis of the second plate is 45 degrees with respect to an optical axis of the first plate.

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FIG. 4 is a schematic diagram illustrating an embodiment of a polarization transformer having three plates wherein the orientation of an optical axis of the second plate is 45 degrees with respect to an optical axis of the first and third plates.

FIG. 5 is a schematic diagram illustrating a polarization transformer disposed
5 between a pair of GRIN lenses and input and output optical fibers.

FIG. 6 is a schematic block diagram of a polarization mode dispersion control circuit.

FIG. 7 is a schematic block diagram of a controller circuit.

FIG. 8 is a diagram illustrating an embodiment of a polarization transformer
10 having four plates in a device package.

DETAILED DESCRIPTION OF THE INVENTION

Polarization direction is a term which refers to the angular orientation of a polarization plane with respect to some external reference plane and not to a direction of travel. Electrical phase shift can be expressed in degrees or radians.
15 Degrees are used herein, but should not be confused with angular orientations.

An embodiment of a single plate polarization transformer 20 is shown in FIG. 1. A radiation beam travels from left to right in the figure and passes through a plate 10. In general, the polarization state of a radiation beam can be defined by two parameters, θ and ϕ , where θ defines the relative magnitudes of orthogonal
20 components and ϕ defines their relative phase. The operation of the single plate 10 is such that input radiation having a constant state of polarization SoP (θ_i, ϕ_i) is incident on the plate. The output radiation is shown having an output state of polarization SoP (θ_o, ϕ_o). With a voltage applied to electrodes of the plate (described further herein), those components that are polarized along the slow (S)
25 and fast (F) axes, as described below, are retarded in optical phase by different amounts as they travel through the plate's thickness w . The effects may be visualized as rotating the polarization direction of the beam. When a half-wave voltage V_π is applied, the component polarized along the fast axis becomes 180° out of phase with the component polarized along the slow axis so that its direction is

reversed. Thus, the plate 10 operates to transform a constant input SoP to an output SoP that is tunable over a range of at least 180 degrees.

There are a number of materials and mechanisms that can be used to provide a polarization transformer which will be discussed in more detail below. Its operation in the embodiment illustrated in FIG. 1 can be explained by assuming an ideal material which, with no voltage applied, has equal indices of refraction for all polarization directions (i.e., isotropic). When a voltage is applied, the applied electric field induces a change in index of refraction (also known as field-induced birefringence) along two principal axes referred to as the fast and slow axes, respectively. The radiation components polarized along the fast and slow axes travel with refractive indices n_F and n_S , respectively. The induced birefringence thus causes a relative phase shift in the components. If the plate has a thickness W , the accumulated phase shift or difference is given by $\Delta\phi = 2\pi (n_F - n_S)W/\lambda$. By adjusting W , $\Delta\phi$ can be made to be π radians = 180° . This means that after traversing the plate, the electric field of one polarization component has the opposite sign relative to the other compared to when they entered the plate. For example, if the incoming polarization direction with respect to the optical axis is β , the outgoing direction is then $180^\circ - \beta$ for $(n_F - n_S)$ positive.

The general requirement for the polarization transformer plate is that, when a voltage is applied, a phase shift is $\Delta\phi$ produced between differing polarization directions. Preferably, the material has a high electro-optic coefficient in order to reduce operating voltages to less than 500 volts. Preferably, the mechanical characteristics allow formation of a bar or plate. Further, the material must be transparent at the wavelength of interest, e.g., between 1200 nm and 1600 nm.

A number of electro-optic materials are available, but many require on the order of kilovolts to obtain an appreciable phase change. These requirements are satisfied by a class of ferroelectric complex oxides which 1) are optically isotropic; 2) have a Curie temperature less than about 300°C , so that electro-optic coefficients are high near room temperature; 3) have a diffusive phase transition, so that the temperature dependence of the electro-optic coefficients is lessened; and 4) which are not permanently poled by moderate electric fields since materials with a low

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Curie temperature that become permanently poled are less stable. Example material systems include lead zirconate titanate (PZT), lanthanum modified PZT (PLZT), lead manganese niobate (PMN), and a solid solution of lead manganese niobate and lead tantalate (PMN-PT). Besides PLZT and PZT, without being an exhaustive list
 5 the following materials may be used: $\text{Pb}(\text{Zr,Ti})\text{O}_3$, $\text{Pb}(\text{Mg,Nb})\text{O}_3$, and a solid solution of $\text{Pb}(\text{Mg,Nb})\text{O}_3$ and PbTaO_3 . More members of this class may be discovered in the future.

High speed electro-optic modulators using such materials are described in International Application No. PCT/US99/07761 filed April 8, 1999 which is a
 10 continuation-in-part of U.S. Application No. 09/158,224 filed September 22, 1998, which claims priority to U.S. Provisional Application No. 60/081,011, filed April 8, 1998, and in addition, claims priority to U.S. Provisional Application No. 60/117,386, filed January 27, 1999, the entire contents of all the above applications being incorporated herein by reference.

15 In general, for any material with an optical path length, D , index of refraction, n , and an applied voltage producing an electric field, ξ , one can write:

$$\Delta L = n\Delta D + D\Delta n = nD[d\xi + \gamma\xi^2 - 0.5n^3(r\xi + R\xi^2)]$$

The four terms on the right represent the piezoelectric, electrostrictive, linear electro-optic (Pockell) and quadratic electro-optic (Kerr) effects with coefficients, d ,
 20 γ , r , and R , respectively. All materials exhibit the effects which depend quadratically on ξ to a greater or lesser extent. There also exist 20 classes of piezoelectric crystals with no center of symmetry that also exhibit the two effects which depend linearly on ξ . In many devices, the range of $\Delta\phi$ required is from 0 to π radians. At π radians, ΔL has change by half a wavelength. Materials are often
 25 characterized by the voltage required to effect such a half wavelength change, the half-wave voltage, V_π .

PLZT with a nominal 9/65/35 La/Pb/Zr composition is a preferred material. This composition is known to be transparent in a range from 450 nm to 7 μm ; see, for example, Lionel M. Levinson, Electronic Ceramics, Chapter 7 (Marcel Dekker,
 30 New York, 1987). It is commercially available as hot pressed ceramic plates from Aura Ceramics (New Hope, Minnesota). In the form of hot-pressed ceramics, it is

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optically isotropic and exhibits little birefringence with zero applied voltage. The electro-optic coefficient is high and the effect is approximately quadratic with voltage. PLZT does not exhibit large linear effects ($d = r = 0$) but has high quadratic coefficients, γ and R . For reference purposes nominal values for PLZT are $n = 2.45$ and $R = 2.53 \times 10^{-16} \text{ m/V}^2$ at $0.88 \text{ } \mu\text{m}$ and $n = 2.3$ and $R = 2.4 \times 10^{-16} \text{ m/V}^2$ at $1.55 \text{ } \mu\text{m}$. PLZT has a polycrystalline structure with crystal sizes ranging from about 5 to 20 microns. The required electric fields are considerably higher than for liquid crystal-based devices, but the response time is much shorter.

An electrode geometry which takes advantage of this material is illustrated by the transverse field configuration illustrated in FIG. 2. A plate 100 is shown which has thin metalized electrodes 102, 104 on the top and bottom surfaces, respectively, of a block section 106 of PLZT material. The top electrode 102 is shown connected to a control voltage V and the bottom electrode is connected to ground. The electric field (designated ϵ) is 90° to the direction of radiation propagation (z -axis). Since the effect is based on the electric field in the material, it is desirable to arrange the electrodes as close together as possible to minimize the control voltage. The electrode gap g can be as small as the beam diameter. For a single-mode fiber, the beam diameter is larger, typically $100 \text{ } \mu\text{m}$ or more, than the fiber core diameter, typically $10 \text{ } \mu\text{m}$, because of beam divergence. In an embodiment, the height h which includes the gap, g , and the thickness of the electrodes, is about $500 \text{ } \mu\text{m}$; the length l is about 2.5 mm ; the width w is about 1.5 mm . This embodiment provides an insertion loss of about 0.2 dB . It will be understood that the particular geometry described is an example and that other device geometries can be used.

Having described the operation of the single plate embodiment in FIG. 1 and the preferred materials for fabricating such a plate, additional polarization transformer embodiments in accordance with the present approach are now described.

An embodiment of a two plate polarization transformer 22 is illustrated in FIG. 3, which show a perspective view of two optical elements 10, 12 with a spacing which can be zero in some cases. A radiation beam travels from left to right in the

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figure and first passes through plate 10 followed by plate 12. The orientation of the optical axes of the plates 10, 12 is 45 degrees with respect to each other. With the two plate polarization transformer 22, a constant input SoP can be transformed to an arbitrary output SoP.

5 An embodiment of a three plate polarization transformer 24 is illustrated in FIG. 4, which show a perspective view of three optical elements 10, 12, 14 with a spacing which again can be zero in some cases. A radiation beam travels from left to right in the figure and passes through consecutive plates 10, 12 and 14. The orientation of the optical axis of the second plate 12 is at 45 degrees with respect to
10 the optical axis of the first and third plates 10 and 14, respectively. The second plate 12, being oriented at 45 degrees, changes the ellipticity but not the azimuth of the incident radiation. The three plate polarization transformer 24 is the most general device of the three types described in that an arbitrary input SoP can be transformed to an arbitrary output SoP.

15 A primary limitation on a particular wavelength arises because of the need for material transparency. In addition, since the plates are a fixed thickness, the phase delay will change with the wavelength and, as a secondary effect, the index of refraction changes with wavelength. Thus, performance of the polarization
20 transformer can gradually degrade as wavelengths different from the nominal wavelength are used.

For use with fiber optic communications applications, it is usually desirable to make polarization transformers as small as possible. A configuration which adds several components is illustrated in FIG. 5. Input radiation is provided by optical fiber 202 and output through optical elements 206, 210, 212, 214, 208 to fiber 204.
25 Following fiber 202 is a GRaded INdex (GRIN) lens 206 which functions as a collimator in front of a three plate polarization transformer comprising plates 210, 212, 214. A second GRIN lens 208 is used to collimate radiation output from the third plate 214 in front of output fiber 204.

A control approach for the foregoing polarization transformer embodiments
30 uses precise setting of the applied control voltage(s) to achieve a desired output SoP. In such an approach, the control voltages are set in response to a correction signal

generated by a sensing device coupled to the output of the transformer. The sensing device monitors one or more parameters of the output radiation (e.g., polarization state, signal spectrum) and feeds back an error signal to the control logic which adjusts the control voltages. The nature of the monitored parameters depends on the application.

As noted in the background, typical optical fibers do not preserve the state of polarization which can contribute to the degradation of optical communication signals. This problem becomes even more significant as transmission rates increase. To counter this polarization mode dispersion, a polarization transformer can be used to actively adjust the polarization state of the incoming light signal and thereby correct for the mode dispersion.

Referring now to FIG. 6, a control circuit for use in controlling polarization mode dispersion is shown. The circuit includes a polarization transformer 302, a differential group delay (DGD) 304, a sensor 306 in a transmission path from left to right in the figure, and a control logic block 308 in a feedback path from the sensor 306 to the polarization transformer 302 and group delay 304. The polarization transformer rotates the SoP of the incoming light signal to match the axes of the DGD. The light propagates through the DGD such that the path length for one polarization component is different and adjustable with respect to the other polarization component. When this difference is equal in magnitude and opposite in sign of that in the network, the polarization mode dispersion is fully compensated.

The control approach applies in a similar manner to a coherent detection system in which a locally generated laser light beam is added to the signal-carrying beam and detected by a square law detector that generates a beat signal. The strength of the beat signal depends on the polarization state of the two beams. The polarization state can vary between 0 and a maximum value depending on whether the two beams are orthogonally polarized or parallel to each other. In such an application, the monitored parameter can be the signal level at the modulation frequency relative to the optical power. Initially the polarization state is set to maximize this ratio and the control logic tracks changes in the polarization state so that the output polarization is kept constant.

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Referring to FIG. 7, an embodiment of a controller circuit for controlling a polarization transformer of the present invention is shown. For example, such a controller circuit can be used as the control logic block 308 (FIG. 6).

The controller circuit includes analog input section 402, control circuit 404,
5 EEPROM 406, JTAG (Joint Test Action Group) interface 408, digital signal processor (DSP) 410, power supply 412, analog output 414, RAM 416, clock 418 and high voltage converter 420.

The analog input section 402 receives sensor input signals 403 corresponding to monitored parameters such as polarization state, signal spectrum, or temperature.
10 These sensor inputs are conditioned by control circuit 404 and converted to digital signals for input to the DSP 410. Based on a suitable control algorithm programmed into the DSP for the particular polarization transformer embodiment, the sensor inputs are used to determine appropriate analog output signals 415 that are applied to the plate electrodes through high voltage converter 420 (preferably in the range of
15 200-300V).

Referring to FIG. 8, an embodiment of a polarization transformer device 500 is shown. The device 500 includes four plates 510, 512, 514, 516, a pair of collimators 506, 508, and a device package 520. Input radiation is provided by optical fiber 502 and passes through the optical elements 506, 510, 512, 514, 516,
20 508 to optical fiber 504. The collimators 506, 508 can be GRIN lenses. The plates 510, 512, 514, 516 are shown with relative orientations of the optical axis as 0° , -45° , $+45^\circ$, 0° , respectively. The spacing between plates can be zero in some cases. It should be understood from the foregoing description that additional polarization transformer configurations employing any number of plates can be considered and
25 the plates oriented based on desired output polarization.

While this invention has been particularly shown and described with references to preferred embodiments thereof, it will be understood by those skilled in the art that various changes in form and details may be made therein without departing from the scope of the invention encompassed by the appended claims.

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CLAIMS

What is claimed is:

1. A polarization transformer comprising:
a plate comprising transparent material having an optical axis
oriented perpendicular to a propagation direction of radiation incident upon
the plate that has a first polarization state, the plate having electrodes for
applying an electric field across a plane of the plate perpendicular to the
propagation direction to provide phase change such that the polarization of
radiation transmitted through the polarization transformer is transformed
from the first polarization state to a second polarization state.
2. The polarization transformer of Claim 1 wherein the plate comprises lead
lanthanum zirconate titanate (PLZT) material.
3. The polarization transformer of Claim 1 wherein the plate comprises
transparent ceramic material.
4. The polarization transformer of Claim 1 wherein the plate comprises a
ferroelectric complex oxide.
5. The polarization transformer of Claim 1 wherein the plate is isotropic in the
absence of an applied electric field across the plate electrodes.
6. The polarization transformer of Claim 1 wherein an electric field
corresponding to an applied voltage less than 400 volts provides a phase
retardation of about 180 degrees.

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7. The polarization transformer of Claim 1 further comprising a pair of GRIN lenses disposed in a propagation path of the radiation such that the plate is disposed between the pair.
8. A polarization transformer comprising:
 - 5 at least one plate comprising transparent polycrystalline material having an optical axis oriented perpendicular to a propagation direction of radiation incident upon the polarization transformer that has a first polarization state, the at least one plate having electrodes for applying an electric field across a plane of the plate perpendicular to the propagation
 - 10 direction to provide phase change such that the polarization of radiation transmitted through the polarization transformer is transformed from the first polarization state to a second polarization state.
9. The polarization transformer of Claim 8 wherein the at least one plate comprises first and second plates disposed such that the incident radiation is
- 15 transmitted through the two plates and wherein the orientation of an optical axis of the second plate is at 45 degrees with respect to the optical axis of the first plate.
10. The polarization transformer of Claim 8 wherein the at least one plate comprises first, second and third plates disposed such that the incident
- 20 radiation is transmitted through the three plates and wherein the orientation of an optical axis of the second plate is at 45 degrees with respect to the optical axis of the first and third plates.
11. The polarization transformer of Claim 8 wherein the first polarization state is a first arbitrary polarization state and the second polarization state is a second
- 25 arbitrary polarization state.

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12. The polarization transformer of Claim 8 wherein the at least one plate comprises lead lanthanum zirconate titanate (PLZT) material.
13. The polarization transformer of Claim 8 wherein the at least one plate comprises transparent ceramic material.
- 5 14. The polarization transformer of Claim 8 wherein the at least one plate comprises a ferroelectric complex oxide.
15. The polarization transformer of Claim 8 wherein the radiation is transmitted along a single propagation path through the at least one plate.
16. A polarization transformer comprising:
 - 10 at least one plate comprising lead lanthanum zirconate titanate (PLZT) material having an optical axis oriented perpendicular to a propagation direction of radiation incident upon the polarization transformer that has a first arbitrary polarization state, the at least one plate having electrodes for applying an electric field across a plane of the plate
 - 15 perpendicular to the propagation direction to provide phase change such that the polarization of radiation transmitted through the polarization transformer is transformed from the first arbitrary polarization state to a second polarization state.
17. The polarization transformer of Claim 16 wherein the second polarization
20 state is a second arbitrary polarization state.

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18. The polarization transformer of Claim 16 wherein the at least one plate comprises first, second and third plates disposed such that the incident radiation is transmitted through the three plates and wherein the orientation of an optical axis of the second plate is at 45 degrees with respect to the optical axis of the first and third plates.
19. The polarization transformer of Claim 16 wherein the at least one plate comprises first, second, third and fourth plates serially disposed such that the incident radiation is transmitted through the four plates and wherein the relative orientations of an optical axis of the four plates is 0° , -45° , $+45^\circ$, 0° , respectively.
20. A polarization transformer comprising:
a polarization transformer having at least one plate comprising transparent polycrystalline material having an optical axis oriented perpendicular to a propagation direction of radiation incident upon the polarization transformer that has a first polarization state, the at least one plate having electrodes coupled to a control voltage for applying an electric field across a plane of the plate perpendicular to the propagation direction to provide phase change such that the polarization of radiation transmitted through the polarization transformer is transformed from the first polarization state to a second polarization state; and
a control circuit coupled to the polarization transformer that provides the control voltage to control the phase change.
21. The polarization system of Claim 20 further comprising an input optical fiber coupled to an input optical coupling and an output optical fiber coupled to an output optical coupling, the polarization transformer coupled between the input and output optical couplings.

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22. The polarization system of Claim 20 further comprising a sensor coupled to the output of the polarization transformer for providing a correction signal wherein the control circuit is responsive to the correction signal to adjust the control voltage.
- 5 23. The polarization system of Claim 22 further comprising a differential group delay coupled between the output of the polarization transformer and the sensor for compensating polarization mode dispersion.
24. The polarization system of Claim 20 wherein the at least one plate comprises lead lanthanum zirconate titanate (PLZT) material.
- 10 25. The polarization system of Claim 20 wherein the at least one plate comprises transparent ceramic material.
26. The polarization system of Claim 20 wherein the at least one plate comprises a ferroelectric complex oxide.
- 15 27. The polarization system of Claim 20 wherein the control circuit includes an analog input section for receiving a correction signal, a processor programmed to determine an analog output signal from the correction signal and a high voltage converter for converting the analog output signal to the control voltage.

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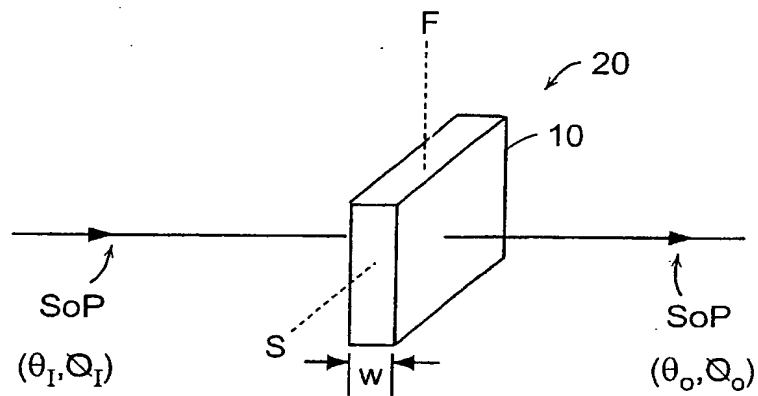


FIG. 1

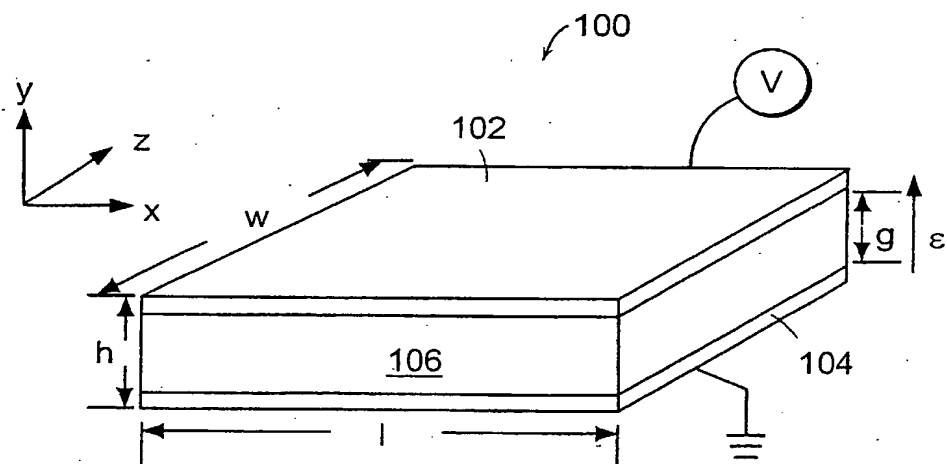
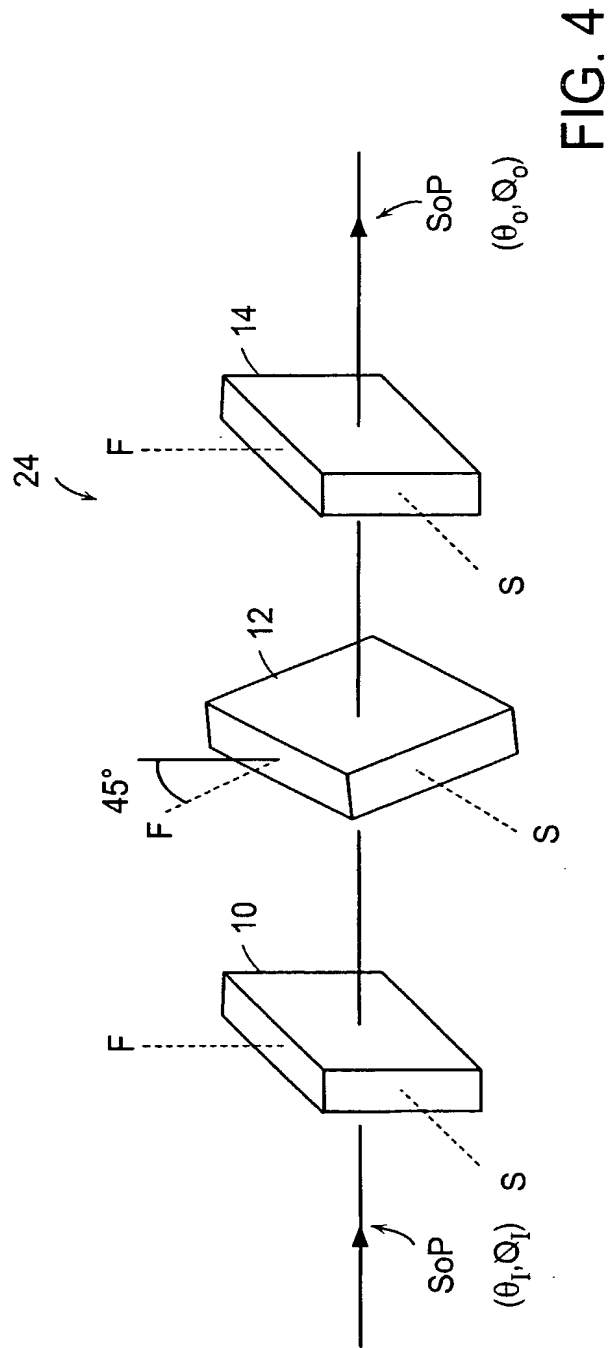
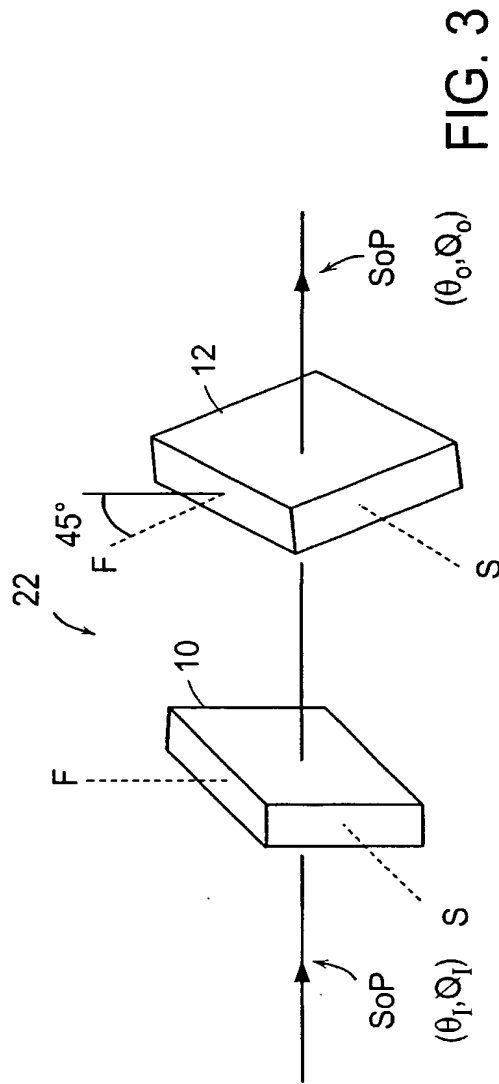


FIG. 2



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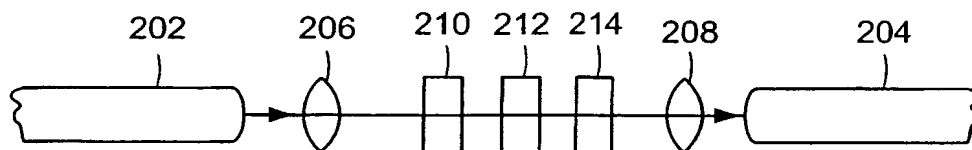


FIG. 5

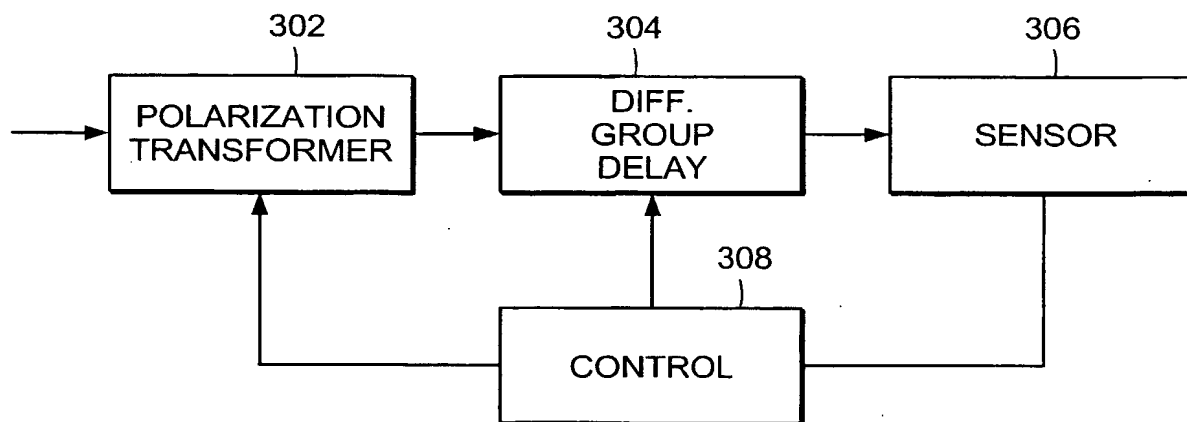


FIG. 6

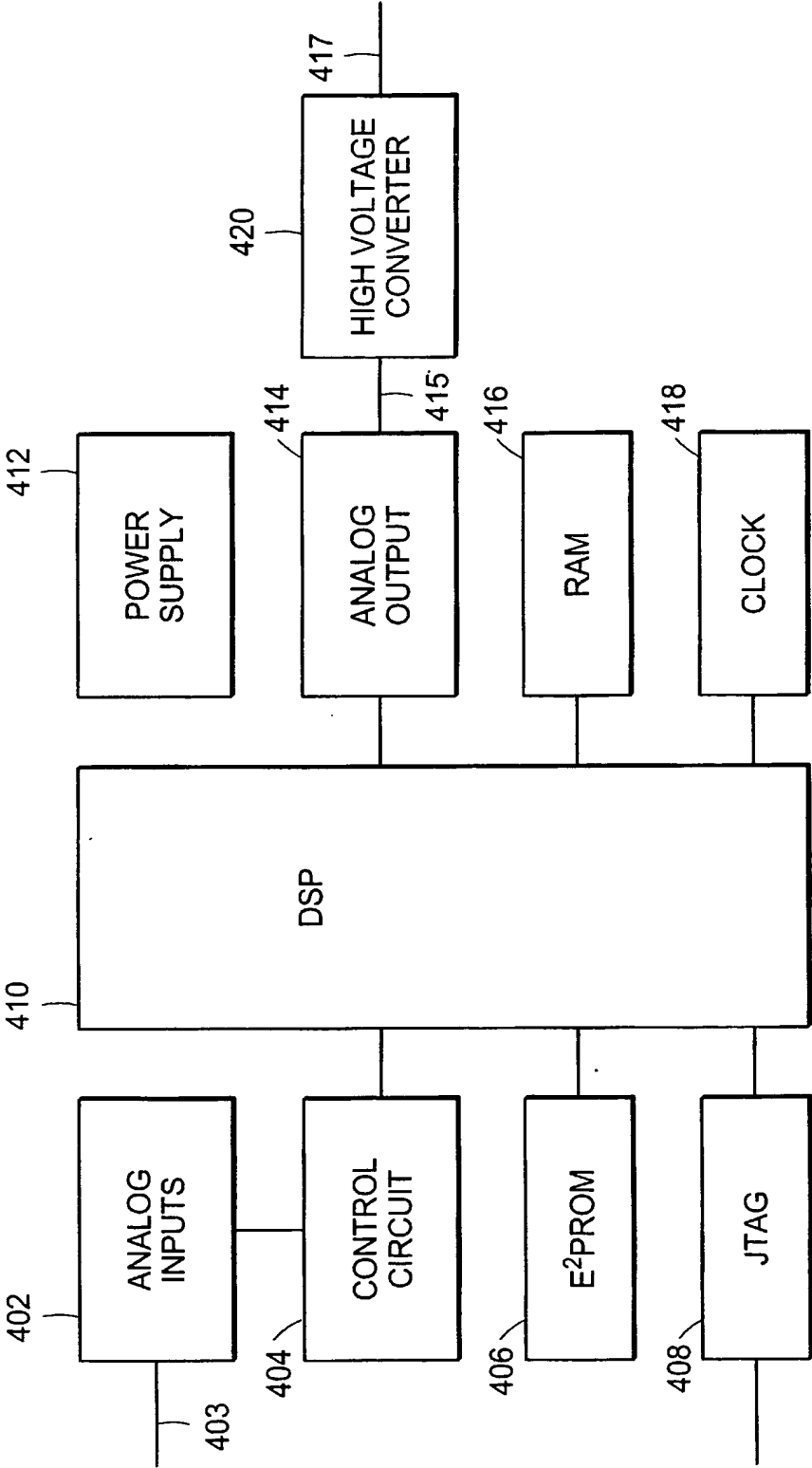


FIG. 7

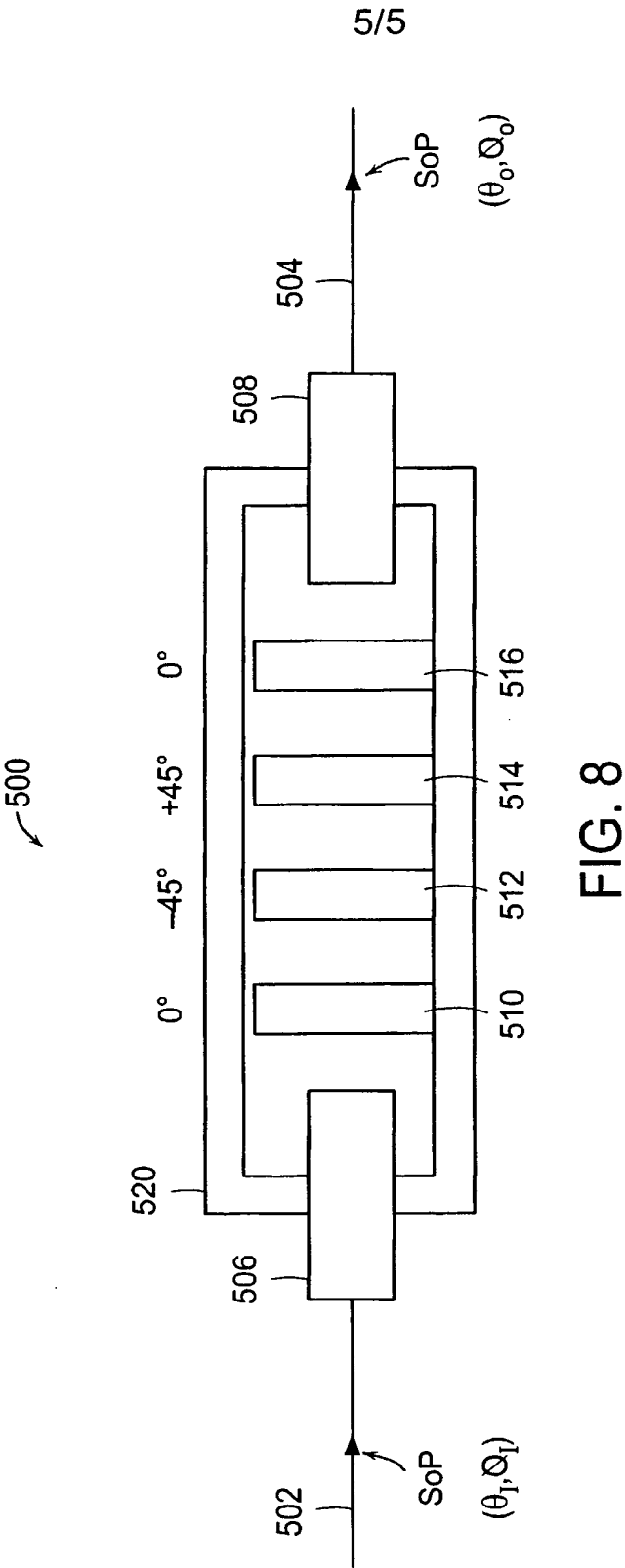


FIG. 8

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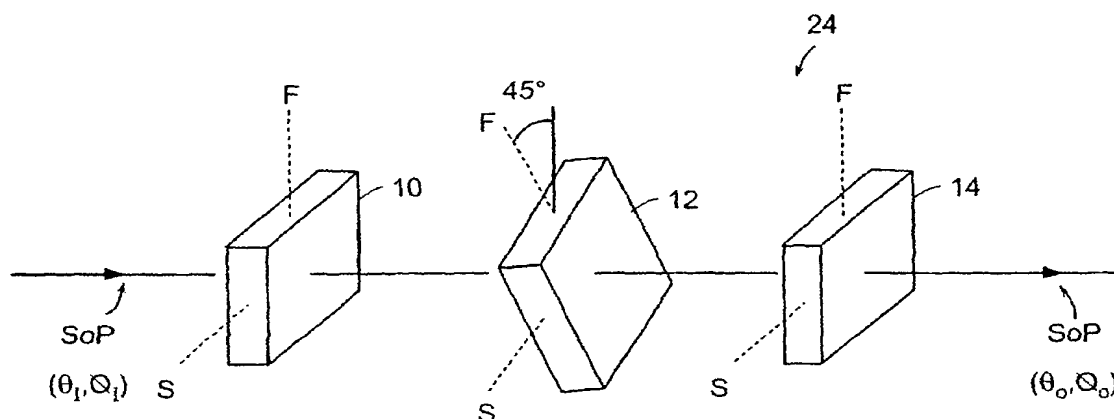
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For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

(54) Title: POLARIZATION TRANSFORMER



(57) Abstract: A polarization transformer includes at least one plate of transparent polycrystalline material which has an optical axis oriented perpendicular to a propagation direction of incident radiation having a first polarization state. The plate includes electrodes for applying an electric field across a plane of the plate perpendicular to the propagation direction so as to provide controlled phase change such that the polarization of radiation transmitted through the polarization transformer is transformed from the first polarization state to a second polarization state. The plate in a preferred embodiment comprises a ferroelectric complex oxide such as lead lanthanum zirconate titanate (PLZT) material. Such a material provides devices that have very fast response (on the order of microseconds) and low insertion loss.

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INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 01/07297

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 G02F1/01 G02F1/055

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 G02F

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

PAJ, INSPEC, EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	PATENT ABSTRACTS OF JAPAN vol. 013, no. 057 (P-825), 9 February 1989 (1989-02-09) & JP 63 246720 A (NEC CORP), 13 October 1988 (1988-10-13) abstract	1-6, 8, 11-17, 20, 21, 24-26
Y	---	9, 10
X	PATENT ABSTRACTS OF JAPAN vol. 011, no. 378 (P-645), 10 December 1987 (1987-12-10) & JP 62 148923 A (NEC CORP), 2 July 1987 (1987-07-02) abstract	1, 8

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Further documents are listed in the continuation of box C.



Patent family members are listed in annex.

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Date of the actual completion of the international search

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INTERNATIONAL SEARCH REPORT

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C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category "	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	<p>SANDEL D ET AL: "10-Gb/s PMD compensation using deformed-helical ferroelectric liquid crystals"</p> <p>24TH EUROPEAN CONFERENCE ON OPTICAL COMMUNICATION. ECOC '98 (IEEE CAT. NO.98TH8398), PROCEEDINGS OF ECOC '98 - 24TH EUROPEAN CONFERENCE ON OPTICAL COMMUNICATION, MADRID, SPAIN, 20-24 SEPT. 1998,</p> <p>pages 555-556 vol.1, XP002177404</p> <p>1998, Madrid, Spain, Telefonica, Spain</p> <p>ISBN: 84-89900-14-0</p> <p>figure 3</p> <p>---</p>	20,22,23
X	<p>SHIMIZU H ET AL: "Endless polarisation controller using electro-optic waveplates"</p> <p>ELECTRONICS LETTERS, 31 MARCH 1988, UK, vol. 24, no. 7, pages 412-413,</p> <p>XP002175879</p> <p>ISSN: 0013-5194</p> <p>the whole document</p> <p>---</p>	1,8,9, 20,24-27
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Y	<p>EP 0 663 604 A (AT & T CORP)</p> <p>19 July 1995 (1995-07-19)</p> <p>column 5, line 26 -column 6, line 41;</p> <p>figure 3</p> <p>-----</p>	9,10

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Information on patent family members

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